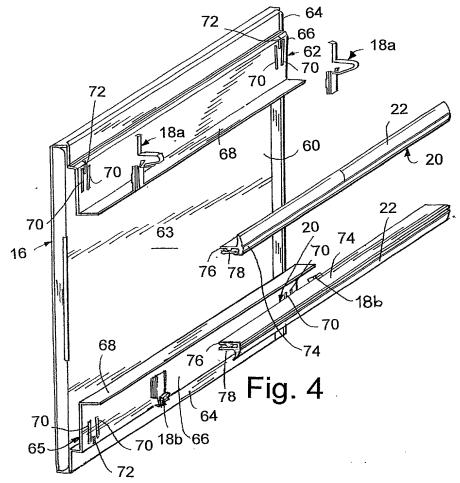
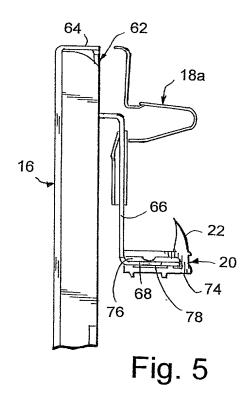
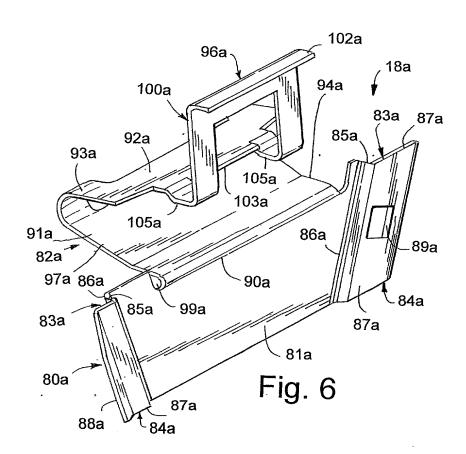
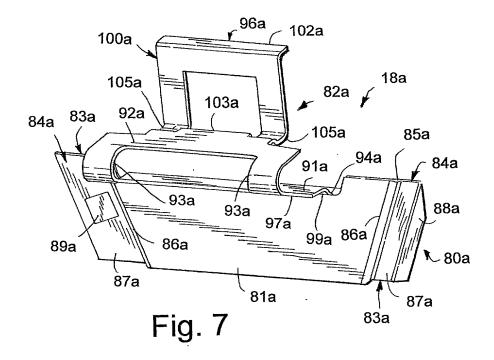


Fig. 3









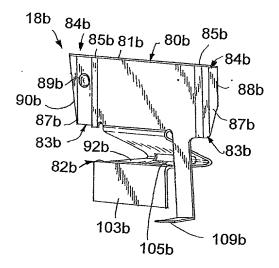
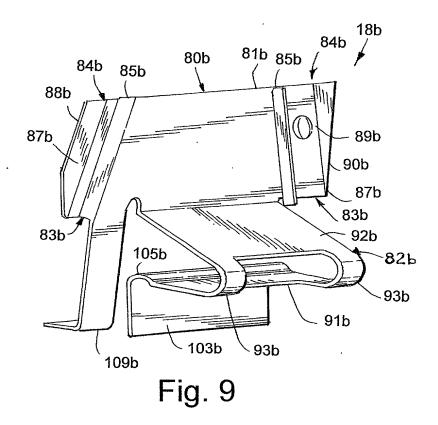
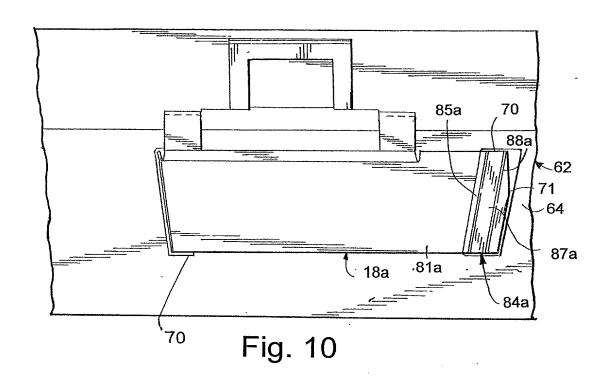


Fig. 8





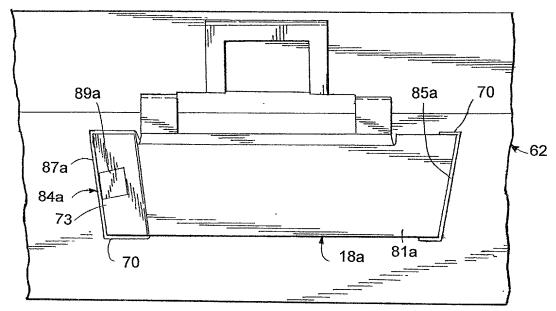


Fig. 11

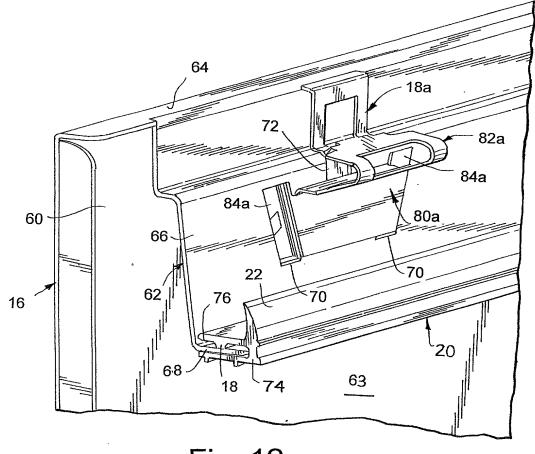
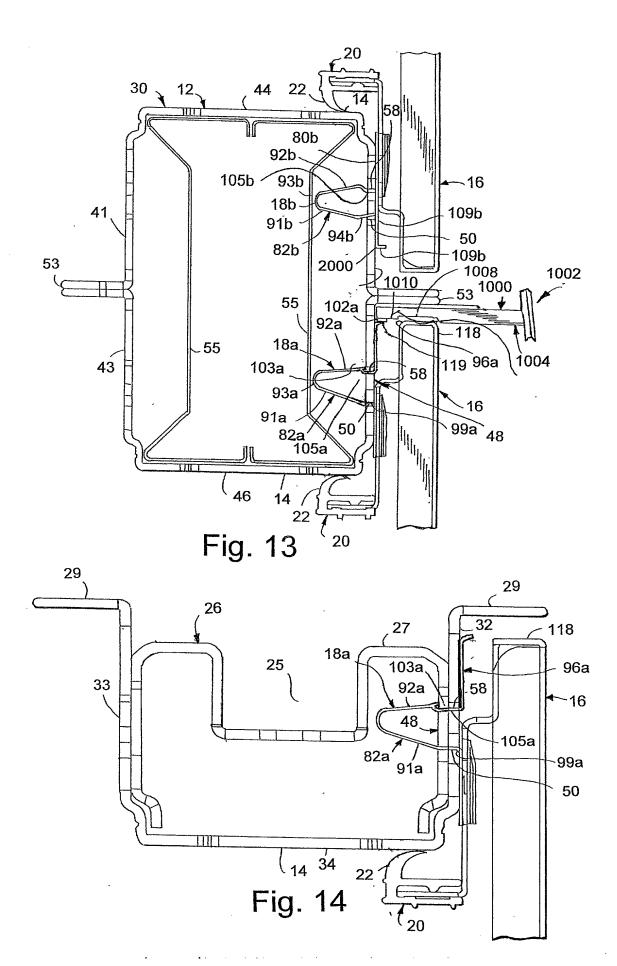
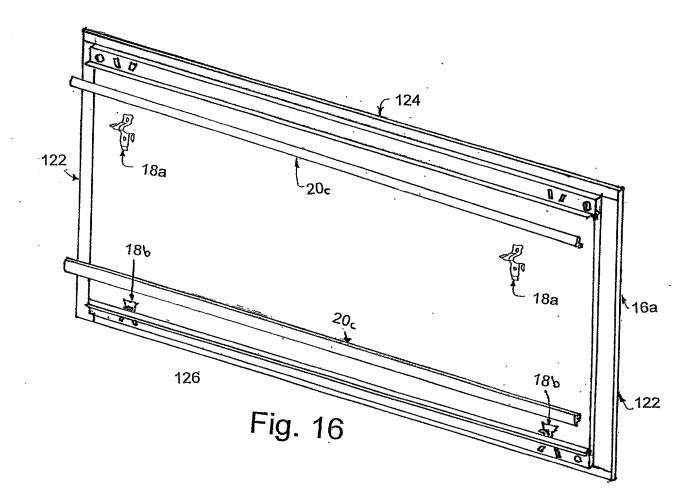
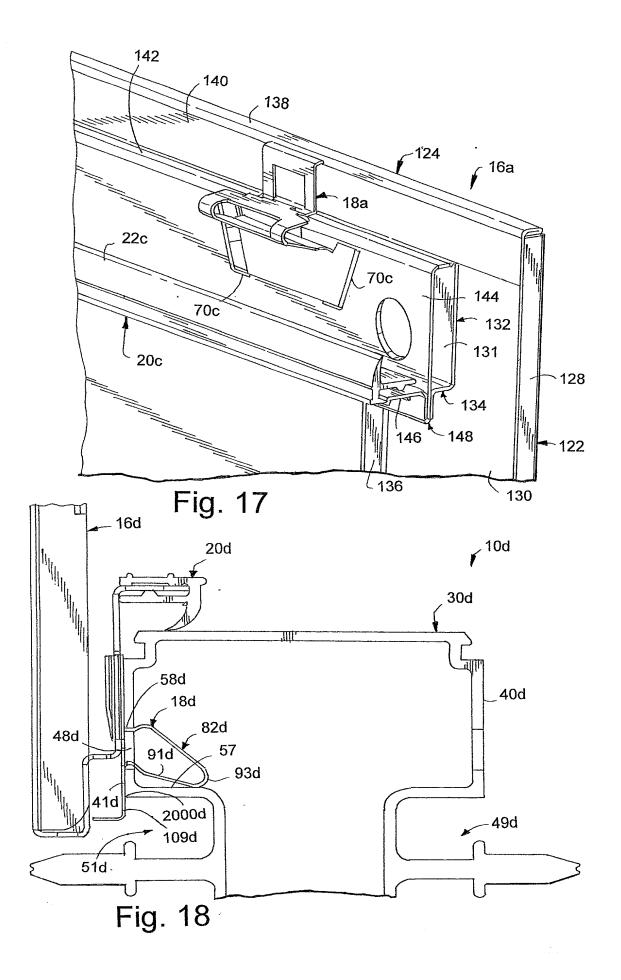
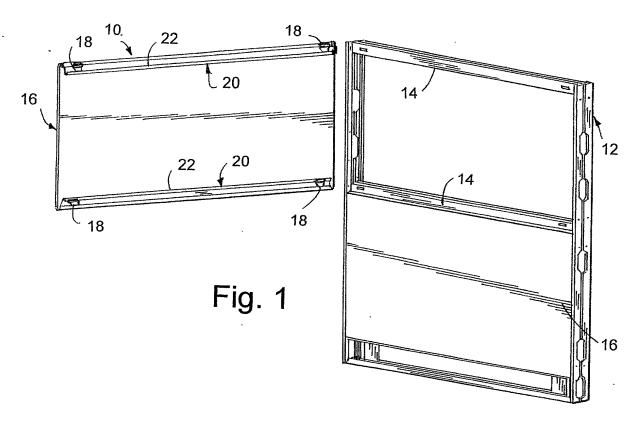


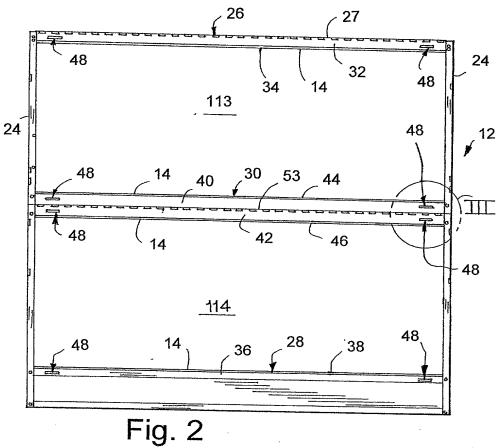
Fig. 12

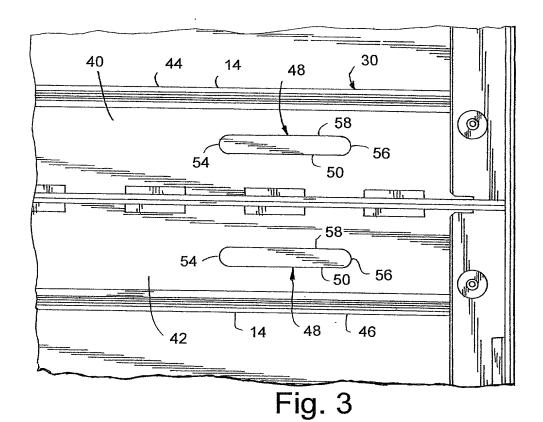




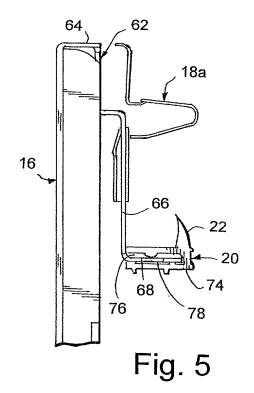


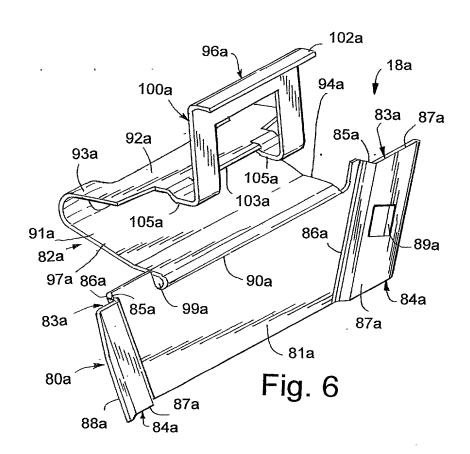


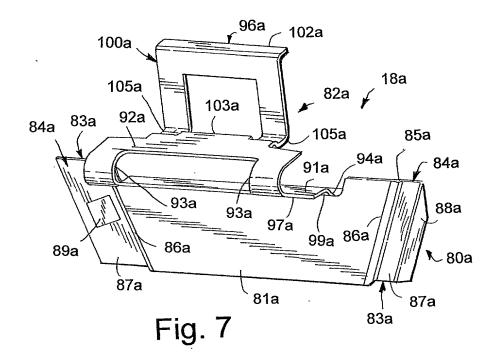




.66 - 62 Î /70 76 78 18b - 70 7₇₈ Fig. 4 70. 70 18b 66







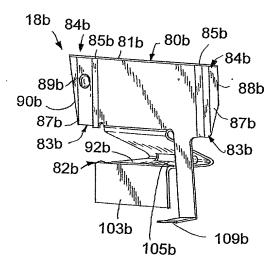
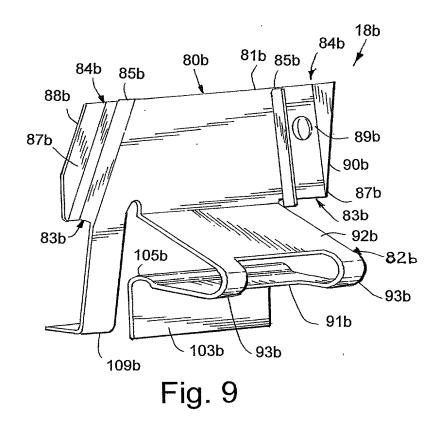
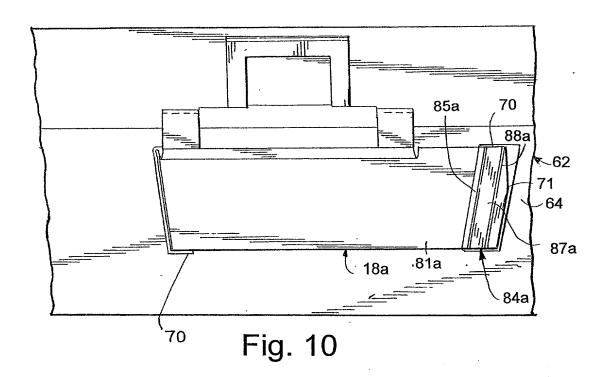


Fig. 8





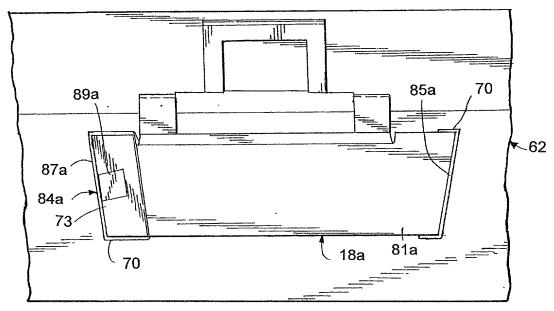


Fig. 11

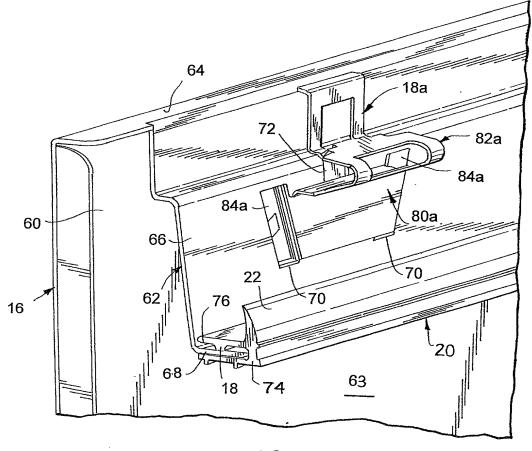


Fig. 12

